Modelling LNG vaporisation rate following release

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Facts & Projections

- Natural gas is one of the fastest growing sectors of energy market; by some accounts entering 'golden age';
- demand for natural gas by 2035 is expected to be 50% higher than today.
- currently approximately quarter of natural gas is transported as LNG;
- Some forecasts indicate that the world trade in LNG is to double by 2035;

New Developments

- Nature of LNG trading is rapidly changing
- The clash between the two structural models of the international LNG industry the traditional, risk-averse, contract dependent model and the free market trading model

Floating LNG developments are gathering speed driven by the need to exploit stranded offshore gas fields



- increase in the amount of LNG transported & the complexity of trading will invariable increase a risk of accidental spillage;
- renewed pressure on improved quantification of risk associated with LNG transport and loading operations;
- Although the track record of LNG industry is very good the regulators remain unconvinced;

What happens when LNG is accidentally spilled on water or soil?

- spreading;
- rapid vaporisation;
- formation of the dense vapour cloud; possibility of pool fire;
- dispersion of the vapour cloud; asphyxiating and highly flammable;
- possibility of flash fire, fireball or destructive explosion

In accidental cryogen spills one of the crucial factors that determines the formation and the future behaviour of the hazardous vapour cloud is the rate of vaporisation of LNG.



$$\frac{dM}{dt} = -\frac{\pi R^2 q}{L}$$

$$q = h(T_w - T_B)$$

$$\frac{dR}{dt} = 1.64 \left[\frac{g(\rho_w - \rho)}{\pi \rho_w \rho} \right]^{\frac{1}{2}} \frac{\sqrt{M}}{R}$$

Assumptions

methane spill

the water surface temperature remains constant throughout the spill duration;
the boiling occurs in the film boiling regime;
heat transfer coefficient remains constant throughout the spill duration;

$$t_{\text{max.}} = 1.0562 \left[\frac{\pi \rho_w \rho_{C1} L_{C1}^2 M_0}{g(\rho_w - \rho_{C1}) h^2 (T_w - T_{C1})^2} \right]^{1/2}$$



Heat Transfer

$$\frac{\partial T_i}{\partial t} = \kappa_i \frac{\partial^2 T_i}{\partial z^2}$$



$$\frac{\partial T_{w}}{\partial t} = \kappa_{w} \frac{\partial^{2} T_{w}}{\partial z^{2}}$$

 $Z > \mathcal{E}$

$$\rho_{w}L_{w}\frac{\partial \varepsilon}{\partial t} = \lambda_{i}\frac{\partial T_{i}}{\partial z}\Big|_{z=\varepsilon} - \lambda_{w}\frac{\partial T_{w}}{\partial z}\Big|_{z=\varepsilon}$$



How quickly does ice form?



Rate of ice formation & Surface temperature



Ice thickness





Size of enclosure



Compositional influence

- Treat LNG as C_1 - C_2 mixture
- Preferential evaporation of methane
- Phase equilibria calculations have to be performed
- Latent heat will no longer be constant, but will vary as a function of composition
- LNG boiling temperature will increase as vaporization progresses.













Conclusions

- the rate of vaporization of LNG on water is a strong function of the surface temperature of water.
- the formation of an ice layer will have a profound effect upon the vaporization rate leading to much longer evaporation times.
- this can have important consequences on assessing risk associated with LNG spill.
- when predicting real life scenarios based on scaled up laboratory data, the extent of ice formation needs to be taken into account and modelled accordingly.
- treating LNG as pure methane will result in overestimation of the vaporisation rates in the latter stages of the spill and wrong dynamics;

Key Research Issues

- Modelling transitional boiling, especially the heat transfer coefficient; Both theory & experiments needed
- Scale-up of lab experiments & making use of experimental data in large spills;
- Influence of surface roughness on heat transfer (larger surface area, break-up of the pool;)
- Modelling effective heat transfer through water